# KRNE-TV <br> 1,022-Foot Guyed Tower <br> Merriman, Cherry County, Nebraska Nebraska Educational Telecommunications 

Structural Analysis Report<br>January 25, 2021

Analysis and Report by: Jiantao Yu, P.E. (SC)
Checked by: Moses Berry, P.E. (SC)
Reviewed by: Jean Lecordier, P.E. (SC)

TCI Project No. 21.331.001


January 25, 2021

## Nebraska Educational Telecommunications <br> 1800 North $33^{\text {rd }}$ Street <br> Lincoln, NE 68503

## Attention: Mr. Chris Homer

## Re: Structural Analysis of Existing <br> KRNE-TV 1,022-Foot Guyed Tower <br> Merriman, Cherry County, Nebraska <br> TCI Project \# 21.331.001 <br> Proposed Loading for KRNE-TV

Dear Mr. Homer,
We are pleased to submit our report for the structural analysis of the above referenced guyed tower to support the required antenna loading as listed in section 3.

The guyed tower will require upgrades for Load Case 1 \& Load Case 2 in order to conform to the requirements of ANSI/TIA-222-H Standard for a $112-\mathrm{mph}$ wind with no ice and seismic loading using $\mathrm{S}_{\mathrm{s}}=0.194$, with the required antenna loading. A preliminary design revealed the following modification requirement for Load Case 1 \& Load Case 2: Reinforce outer guy anchors and adjust guy wire initial tension.

The analysis was performed using Structure Class II, Exposure Category C, Topographic Category 1 and an $\mathrm{S}_{\mathrm{s}}=0.194$ as design criteria from the ANSI/TIA-222-H Standard. Wind loading, ice and seismic parameters were obtained using ASCE 7 Hazards report for ASCE/SEI 7-16.
After the recommended upgrades are performed, the guyed tower and foundations will conform to the requirements of ANSI/TIA-222-H Standard for Load Case 1 \& Load Case 2 for a 112mph wind with no ice and seismic loading using $\mathrm{S}_{\mathrm{s}}=0.194$, with the required antenna loading.

Should you have any questions or wish to discuss any aspect of this report, please do not hesitate to contact TCI.

Sincerely,


Jiantao Yu, P.E. (SC)
Senior Project Engineer
Tower Consultants, Inc.


## 1. Authorization/Purpose

As authorized, Tower Consultants, Inc. (TCI) has completed a structural analysis of the existing 1,022-foot guyed tower located in Merriman, Nebraska. The analysis was performed per the request by Mr. Chris Homer of Nebraska Educational Telecommunications to determine the feasibility of the tower to support the required antenna loading as listed in section 3.

## 2. Tower History

The 1,022-foot three sided guyed tower located in Merriman, Nebraska was originally designed by Dresser in 1968 in accordance with the EIA RS-222-A Standard for a basic wind pressure of 50-psf with no ice.

The current structural analysis was performed on the basis that the information used is accurate. This information may consist of, but not limited to:

- Information supplied by the customer,
- Information supplied by potential tenant and/or tower owner,
- Information from documents or drawings available to TCI, or
- Information acquired during a field inspection mapping by National Tower Controls dated March 10, 2020.

All information used is as depicted in the attached appendices.
TCI did not perform a field inspection and mapping to verify the location and information about the current equipment on the tower. The locations and specifics of all equipment used for the loading of this analysis are based on information and photographs provide to TCI. Any deviation from the information and assumptions made in this analysis would void the results of the analysis.

## 3. Conditions Investigated

This analysis was performed to determine the feasibility of the tower to support the following antenna loading:

| Elevation (ft.) | Equipment | Tx Line |
| :---: | :---: | :---: |
| 952-1,022 | (1) Dielectric TW-12B12-R | (1) $4-1 / 16 "$ rigid <br> (1) 1" deicer conduit |
| 913.5 | (1) Platform (SE face) | -- |
| 885 | (3) OBS lights | (1) 1" conduit* |
| 878 | (1) 12-bay FM antenna (S leg)** | (1) 3-1/8" rigid |
| 735 | (3) OBS lights | (1) 1" conduit* |
| 585 | (1) Beacon | (1) 1" conduit* |
| 508 | (1) 4-bay FM antenna (S leg) | (1) 7/8" flex |
| 485 | (1) Ice shield (S leg) | -- |
| 475 | (4) Yagi antennas (S leg) | (1) 7/8" flex |
| 442 | (1) Ice shield (NE leg) | -- |
| 440 | (3) OBS lights | (1) 1" conduit* |
| 438 | (1) 3' HP dish (NE leg) | (1) $1 / 2$ " flex |
| 414 | (1) Dipole antenna (NW leg) | (1) $7 / 8$ " flex |
| 413 | (1) Dipole antenna (NE leg) | (1) 7/8" flex |
| 364 | (1) Dipole antenna (NE leg) | (1) 7/8" flex |
| 357 | (1) Ice shield (NW leg) | -- |
| 353 | (1) 3' HP dish (NW leg) | (1) $1 / 2$ " flex |
| 290 | (1) Beacon | (1) 1" conduit* |
| 254 | (1) Dipole antenna (NE leg) | (1) 7/8" flex |
| 237 | (1) Dipole antenna (NE leg) | (1) 7/8" flex |
| 185 | (1) Ice shield (SE face) | -- |
| 185 | (1) Ice shield (W face) | -- |
| 178 | (1) 10' HP dish (SE face) | (1) $1 / 2$ " flex |
| 178 | (1) 10' HP dish (W face) | (1) $1 / 2$ " flex |
| 145 | (3) OBS lights | (1) 1" conduit* |
| 0-413 | -- | (1) 1" conduit |
| 0 - top | Climbing ladder with safety device | -- |

## * Shared conduit

** Equipment to be removed and replaced with:
Load Case 1: New (1) DCRM12CR at 878' with new (1) 3-1/8" rigid
Load Case 2: New (1) DCRM10CR at 878' with new (1) 3-1/8" rigid

## 4. Loads and Stresses

An analysis was conducted in order to assess the structural performance of the tower per the current design standard ANSI/TIA-222-H, "Structural Standards for Antenna Supporting Structures, Antennas and Small Wind Turbine Support Structures". Member stresses, required strength and design strength used to evaluate the adequacy of the structure were in accordance with this standard.

## 5. Method of Analysis

A three-dimensional computer model was created using the TNXTower Version 8.0.7.4 analysis program (Tower Numerics, Inc., 2020). TNXTower is a general-purpose modeling, analysis and design program created specifically for communication towers. The program generates nodes and elements for a finite element analysis (FEA) and determines the pressure coefficients, wind pressures, ice loads and resulting forces on the tower for standard framing types including selfsupporting towers, guyed towers and poles.

## 6. Results

Associated with each loading condition are the tower elevations, member sizes and member stress percentages. The member stress percentage is the ratio of required strength to the nominal strength expressed as a percentage. A stress ratio greater than $100 \%$ denotes an overstress.

The following member stresses were calculated with a basic wind speed of $112-\mathrm{mph}$ with no ice and seismic loading using $\mathrm{S}_{\mathrm{s}}=0.194$ in accordance with ANSI/TIA-222-H Standard with the required antenna loading:

Maximum Member Stresses

| Element | Elevation (ft.) | Maximum \% <br> Load Case 1 | Maximum \% <br> Load Case 2 |
| :---: | :---: | :---: | :---: |
| Guy | 950.5 | $\mathbf{8 1 . 7}$ | $\mathbf{8 1 . 1}$ |
| Leg | $28.5-33.5$ | $106.6^{* *}$ | $106 . \mathbf{4}^{* *}$ |
| Diagonal | $6.75-13.5$ | 90.0 | 90.0 |
| Horizontal | 173.5 | 51.3 | 51.1 |
| Base Foundation | -- | $\mathbf{8 8 . 1}$ | $\mathbf{8 8 . 1}$ |
| Guy Inner Anchor | -- | $\mathbf{9 7 . 7}$ | $\mathbf{9 7 . 7}$ |
| Guy Outer Anchor | -- | $\mathbf{1 1 7 . 7 * *}$ | $\mathbf{1 1 6 . 4 * *}$ |

** Member has unacceptable overstress.

## 7. Conclusions and Recommendations

The tower is overstressed for Load Case 1 \& Load Case 2 with the required antenna loading when subjected to a basic wind speed of $112-\mathrm{mph}$ with no ice and seismic loading using $\mathrm{S}_{\mathrm{s}}=0.194$ in accordance with the ANSI/TIA-222-H Standard.

In order to meet the requirements of ANSI/TIA-222-H Standard for a 112-mph wind with no ice and seismic loading using $\mathrm{S}_{\mathrm{s}}=0.194$ for Load Case 1 \& Load Case 2, we recommend that the following upgrades be performed on the tower prior to installing the proposed equipment:

1. Reinforce outer guy anchors by adding overburden.
2. Adjust the guy wire tensions to the values listed on the following chart:

| Guy Level | Guy Anchor | Existing Guy Tension | Proposed Guy Tension |
| :---: | :---: | :---: | :---: |
|  |  | \% of Ultimate Tension | \% of Ultimate Tension |
| $6^{\text {th }}$ (top) | Outer Anchor | 10.0\% | 14.0\% |
| $5^{\text {th }}$ |  | 10.0\% | 12.0\% |
| $4^{\text {th }}$ |  | 10.0\% | 10.0\% |
| $3^{\text {rd }}$ | Inner Anchor | 10.0\% | 10.0\% |
| $2^{\text {nd }}$ |  | 10.0\% | 10.0\% |
| $1^{\text {st }}$ (bot) |  | 10.0\% | 14.0\% |

Note: Values shown above are valid at 60 degree Fahrenheit; a P\&T chart with temperature correction will be required for field adjustments. It is also assumed that adequate adjustment is available on guy hairpins to achieve the recommended tensions.

The following member stresses were calculated with a basic wind speed of $112-\mathrm{mph}$ with no ice and seismic loading using $\mathrm{S}_{\mathrm{s}}=0.194$ in accordance with ANSI/TIA-222-H Standard with the required antenna loading after the upgrades mentioned above have been implemented:

Maximum Member Stresses

| Element | Elevation (ft.) | Maximum \% <br> Load Case 1 | Maximum \% <br> Load Case 2 |
| :---: | :---: | :---: | :---: |
| Guy | 950.5 | $\mathbf{8 4 . 6}$ | $\mathbf{8 4 . 0}$ |
| Leg | $28.5-33.5$ | 96.5 | 96.4 |
| Diagonal | $358.5-363.5$ | 92.1 | 92.1 |
| Horizontal | 173.5 | 51.4 | 51.4 |
| Base Foundation | -- | $\mathbf{8 8 . 1}$ | $\mathbf{8 8 . 1}$ |
| Guy Inner Anchor | -- | $100.8^{*}$ | $\mathbf{1 0 0 . 8}$ |
| Guy Outer Anchor | -- | $\mathbf{8 9 . 3}$ | $\mathbf{8 9 . 3}$ |

* Member has acceptable overstress.

Tower member detail drawings were not available. Therefore, an analysis was not performed on the member connections. However, it is common practice to design the member connections to a factor of safety that exceeds the capacity of the member. With the existing and the proposed loading, the tower member stresses are still within the allowable limits. Therefore, it may be concluded that the member connections appeared to be adequately sized for the existing and the proposed loading.

The following table summarizes the maximum foundation reactions after the upgrades mentioned above have been implemented:

Maximum Foundation Reactions

| Foundation Reactions | Load Case 1 ANSI/TIA-222-H 112-mph with no ice Seismic $\mathrm{S}_{\mathrm{s}}=0.194$ | Load Case 2 ANSI/TIA-222-H 112-mph with no ice Seismic $\mathrm{S}_{\mathrm{s}}=0.194$ |
| :---: | :---: | :---: |
| Tower Base: <br> Moment <br> Bearing Force <br> Shear Force | $\begin{gathered} 996 \mathrm{ft} \text {-kips } \\ 483 \mathrm{kips} \\ 9 \mathrm{kips} \\ \hline \end{gathered}$ | $\begin{gathered} 995 \mathrm{ft} .-\mathrm{kips} \\ 482 \mathrm{kips} \\ 9 \mathrm{kips} \end{gathered}$ |
| Inner Anchor: Uplift Force Shear Force | 69 kips 98 kips | 69 kips 98 kips |
| Outer Anchor: Uplift Force Shear Force | 96 kips 91 kips | 96 kips 90 kips |

After the upgrades mentioned above are implemented, the guyed tower and foundations will be adequate for the required antenna loading.

## 8. Provisions of Analysis

The analysis performed and the conclusions contained herein are based on the assumption that the tower has been properly installed and maintained, including, but not limited to the following:

1. Proper alignment and plumbness.
2. Correct guy tensions.
3. Correct bolt tightness.
4. No significant deterioration or damage to any component.
5. All equipment, $\mathrm{T} /$ /'s, antennas, etc, is properly secured to the tower per manufacturer's recommendation.
6. All mounts, if applicable, are considered adequate to support the loading.

Furthermore, the information and conclusions contained in this Report were determined by application of the current "state-of-the-art" engineering and analysis procedures and formulae.

Tower Consultants Incorporated assumes no obligation to revise any of the information or conclusions contained in this Report in the event that such engineering and analysis procedures and formulae are hereafter modified or revised. In addition, under no circumstances will Tower Consultants Incorporated have any obligation or responsibility whatsoever for or on account of consequential or incidental damages sustained by any person, firm or organization as a result of any information or conclusions contained in the Report, and the maximum liability of Tower Consultants Incorporated if any, pursuant to this Report shall be limited to the total funds actually received by Tower Consultants Incorporated for preparation of this Report.

Customer has requested Tower Consultants Incorporated to prepare and submit to Customer an engineering analysis with respect to the Subject Tower and has further requested Tower Consultants Incorporated to make appropriate recommendations regarding suggested structural modifications and changes to the Subject Tower. In making such request of Tower Consultants Incorporated, Customer has informed Tower Consultants Incorporated that Customer will make a determination as to whether or not to implement any of the changes or modifications which may be suggested by Tower Consultants Incorporated and that Customer will have any such changes or modifications made by riggers, erectors and other subcontractors of Customer's choice.

Tower Consultants Incorporated shall have the right to rely upon the accuracy of the information supplied by the customer and shall not be held responsible for the Customer's misrepresentation or omission of relevant fact whether intentional or otherwise.

Customer hereby agrees and acknowledges that Tower Consultants Incorporated shall have no liability whatsoever to Customer or to others for any work or services performed by any persons other than Tower Consultants Incorporated in connection with the implementation of services including but not limited to any services rendered for Customer or for others by riggers, erectors or other subcontractors. Customer acknowledges and agrees that any riggers, erectors or subcontractors retained or employed by Customer shall be solely responsible to Customer and to others for the quality of work performed by them and that Tower Consultants Incorporated shall have no liability or responsibility whatsoever as a result of any negligence or breach of contract by any such rigger, erector or subcontractor and that Customer and rigger, erector, or subcontractor will provide Tower Consultants Incorporated with a Certificate of Insurance naming Tower Consultants Incorporated as additionally insured.

## Appendix E-1

## Tower Elevation




Appendix E-2
Cross Section
(1) ${ }^{7} / 8^{\prime \prime}$ LINE TO 508'
(1) ${ }^{7} / 8^{\prime \prime}$ LINE TO $475^{\prime}$
(1) $7 / 8^{\prime \prime}$ LINE TO 414'
(1) 1" LIGHTING CONDUIT
(1) $7 / 8^{\prime \prime}$ LINE TO $413^{\prime}$
(1) $7 / 8^{\prime \prime}$ LINE TO $364^{\prime}$
(1) $1 / 22^{\prime \prime}$ LINE TO $353^{\prime}$
(1) 1" CONDUIT TO 413'
(1) $31 / 8^{\prime \prime}$ RIGID TO 878' (PROPOSED FOR LC \& LC)
CLIMBING LADDER WITH SAFETY DEVICE
(1) ${ }^{1 / 2 "} \mathbf{n}^{\prime \prime}$ LINE TO 438'
(1) $7 / 88^{\prime \prime}$ LINE TO 254'
(1) ${ }^{7} / 8^{\prime \prime}$ LINE TO $237^{\prime}$

(1) $4 \not 1 / 16^{\prime \prime}$ RIGID TO TOP
(1) 1 " CONDUIT TO TOP

NOTE: ANALYSIS IS BASED ON THE ABOVE LAYOUT. ANY DEVIATION FROM ABOVE WILL VOID THIS ANALYSIS.



